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### WATERTOWN ARSENAL **LABORATORY**

#### MEMORANDUM REPORT

NO. WAL 710/713

Comparison of 245T and 755T Aluminum Alloys

on the Basis of Resistance to Perforation

by Fragment-Simulating Projectiles

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BY

J. F. SULLIVAN Asat. Engineer

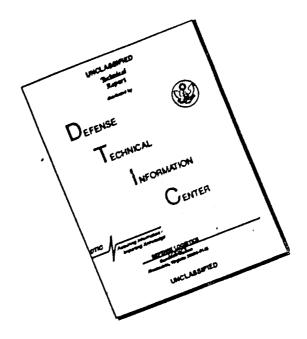
M. A. BROUGH Proof Technician

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DATE 8 January 1945

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WATERTOWN ARSENAL LABORATORY

MEMORANDUM REPORT NO. WAL 710/713

30th Partial Report on Problem B-8.2

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Comparison of 24ST and 75ST Aluminum Alloys

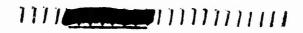
on the Basis of Resistance to Perforation

by Freement-Simulating Projectiles



- 1. At the request of the Office, Chief of Ordnance, tests have recently been conducted at this arsenal on various samples of 24ST and 75ST aluminum alloys which had earlier been subjected to actual fragmentation tests at Aberdeen Proving Ground.
- 2. There appears to be no significant difference in the resistance characteristics of these two alloys with respect to impact with cal. 45 steel-jacketed ball projectiles or with the fragment-simulators G-1-S<sup>2</sup> and G-23. Their resistance to perforation by these projectiles is considerably inferior to that of an equivalent weight of Hadfield manganese steel and their experience in this respect is consistent with that of other aluminum alloys tested previously.
- 3. Two test samples (one 12" x 12" and one 0" m 10"), free of perioditions, were cut out of each sneet received from Aberdeen Proving bround. These samples were clamped rigidly to wooden ballistic frames and the 12" x 12" samples were subjected to impact by cal. .45 steel-jacketed ball projectiles while the 6" x 12" pieces were tested with cal. .22 fragment-simulating projectiles, G-2, and with cal. .30 fragment-simulating projectiles, G-1-S. The results of these tests are shown in Table I.
- 1. 0.0. 400.112/11981 Wtn 100.112/3227 7 November 1914
- 2. WAL 762/247
- 3. WAL 762/253

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4. Although the resistance of individual pieces of 24ST was sometimes higher than that of 75ST it is felt that the results disclose no significant difference between the resistance characteristics of the two alloys under impact of the projectiles employed in these tests. There is apparent, of course, the customary inferiority of these materials to Hadfield manganese steel of equivalent weight under these test conditions. It should be pointed out that this inferiority does not extrapolate to actual service conditions, because, under actual fragmentation tests (in which 20mm, high explosive shell are detonated) the subject materials appear to be superior to Hadfield manganese steel and it is considered that the latter tests are more significant of actual service conditions than any ballistic limit tests currently in use.

M. A. Brough
Proof Technician

J. F. Sullivan
Asst. Engineer

APPROVED:

E. L. Reed

Research Metallurgist

Acting Chief, Armor Section

#### TABLE I

#### Summary of Ballistic Tests Conducted at Watertown Arsenal

#### on Samples of 24ST and 75ST Duralumin Which Had Been

#### Previously Subjected to Fragmentation Tests

#### at Aberdeen Proving Ground

	Sатр1e	Nominal	Actual	Grams/	Equiv. Steel		listic L	
Type	No.	Gauge	Gauge	Sq.Ft.	Gauge	451	G_22	G_1_\$3
75ST	· 8	.156	.15 <sup>4</sup> "	1016"	.055	922		
		W	.154	1008	.054		960 <sup>12</sup> 25	1063#23
	9	.156	.160	1043	.056	847		
-	-		.157	1028	.056		970±5	107727
	2	.156	.156	1022	.055	887	055	100±0-
	11	125	.155	1016	•055	770	955 10	1083-23
*	11	.125	.127 .123	8 <b>3</b> 2 <b>798</b>	.046 .043	772	775 <sup>±</sup> 15	825 <sup>±</sup> 10
*	7	.125	.125	821	•О <del>лл</del>	753	112-12	825-10
×	n	• 129	.125	816	0 <del>/1/1</del>	193	800 <sup>±</sup> 25	803 <sup>±</sup> 23
*	8	.125	.124	821	.044	790	000 -	00) []
<b>K</b>	H	N	.127	838	.045	100	827±17	898 <sup>±</sup> 13
p	1	.102	.100	6 <b>56</b>	.035	522		- , - ,
H	×	N	.101	664	.036		728-13	803 <sup>±</sup> 23
	4	.102	.103	672	.036	537		•
H	Ħ	, #	.102	674	.036		760 <sup>2</sup> 30	720±25
	20	.102	.101	665	.036	541		
-1			.101	662	.036		725*40	723±13
2491	16-4-53	.156	.156	1031	.056	927		
	7 . (0	1-6	-157	1028	.056	#do	1030±10	1025 <b>±</b> 15
	7-4-69	.156	.161	1046	.057	<b>8</b> 80	06=	1042±17
*	13-4-67	.156	.157	1022 1028	.055	929	965	1042-1/
	1)-4-01	.190	.157 .158	1032	.056 .056	ジニフ	983±23	1090±15
×	10_B_179	.125	.124	826	.045	720	707-27	1030-13
×	# T T T T T T T T T T T T T T T T T T T	N	.125	834	.045	,-0	823±27	870±25
×	13-4-136	.125	.124	837	.045	777		010-27
×		N	.128	836	.045	i	825 <sup>±</sup> 10	868 <sup>±</sup> 17
7	13-B-183	.125	.127	837	.045	736		•
•		*	.126	836	.045		835±20	842=27
	16	.102	.104	684	.037	568		
	•		.105	678	.037	4	735 <sup>±</sup> 20	710 <sup>±</sup> 20
	26	.102	.104	685	.037	539	_\	C
-		300	.104	672	.036		740 <sup>±</sup> 25	690 <sup>±</sup> 15
	29	.102	.104 .104	6 <b>88</b> 6 <b>82</b>	.037	522	775400	7),6470
FOR OF	MPARISON:		. 104	002	.035		775 25	745年10
	ald Manganese	Steel		-	.045	950	1675	1050
			<del></del>					

<sup>1.</sup> Cal..45 steel-jacketed ball projectile - 230 grains

<sup>2.</sup> Cal..22 fragment-simulating projectile - 17 grains

<sup>3.</sup> Cal.. 30 fragment-simulating projectile - 34 grains